



Non-linear time-dependent modelling of heterogeneous nuclear reactors

Applications to Xenon oscillations in pressurized water reactors

Master's thesis in Physics

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DEPARTMENT OF PHYSICS CHALMERS UNIVERSITY OF TECHNOLOGY Gothenburg, Sweden 2023 www.chalmers.se

Master's thesis presentation:

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Awarded the 2024 SKC Sigvard Eklund price for best master's thesis

Fredrik Öhrlund, MSc

Outline of Presentation

• My Master Thesis

5 min

Simulating a reactor

3 min

•Xenon-135

7 min

Thesis background

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| project description | |

From Page 1

- In thermal nuclear reactors, there is a fission product called Xenon-135
- Its well known in reactor physics that Xe-135 can cause "xenon oscillations"
- Xenon oscillations are expected to be a more frequent problem in the future
- The DREAM group at Chalmers is currently developing methods for predicting xenon-oscillations
- "This master thesis project aims at developing modelling capabilities that allow for the calculation of the three-dimensional time-dependence of the neutron flux in a nuclear reactor for the specific purpose of studying the xenon effect."
- Unlike proprietary software, will have full access to the source code

Problem definition

$$\frac{1}{v_1} \frac{\partial}{\partial t} \phi_1(\vec{\mathbf{r}}, t) = \left[\vec{\nabla} \cdot D_1(\vec{\mathbf{r}}, t) \vec{\nabla} + \nu \Sigma'_{f,1}(\vec{\mathbf{r}}, t) - \Sigma_{a,1}(\vec{\mathbf{r}}, t) - \Sigma_r(\vec{\mathbf{r}}, t) \right] \phi_1(\vec{\mathbf{r}}, t)
+ \nu \Sigma'_{f,2}(\vec{\mathbf{r}}, t) \phi_2(\vec{\mathbf{r}}, t)
+ \alpha_{1 \to 1}(\vec{\mathbf{r}}) (\phi_1(\vec{\mathbf{r}}, t) - \phi_{eq,1}(\vec{\mathbf{r}})) + \alpha_{2 \to 1}(\vec{\mathbf{r}}) (\phi_2(\vec{\mathbf{r}}, t) - \phi_{eq,2}(\vec{\mathbf{r}}))$$



From Page 2



To summarize the remaining 5 pages of the project description:

"Here is a long list of contraints and requirements...

... please solve these equations, using a computer...

... then...

... somehow perturb the system to generate xenon oscillations"



$$\begin{split} \frac{1}{v_1} \frac{\partial}{\partial t} \phi_1(\vec{\mathbf{r}},t) &= \left[\vec{\nabla} \cdot D_1(\vec{\mathbf{r}},t) \vec{\nabla} + \nu \Sigma'_{f,1}(\vec{\mathbf{r}},t) - \Sigma_{a,1}(\vec{\mathbf{r}},t) - \Sigma_r(\vec{\mathbf{r}},t) \right] \phi_1(\vec{\mathbf{r}},t) \\ &+ \nu \Sigma'_{f,2}(\vec{\mathbf{r}},t) \phi_2(\vec{\mathbf{r}},t) \\ &+ \alpha_{1\to 1}(\vec{\mathbf{r}}) (\phi_1(\vec{\mathbf{r}},t) - \phi_{eq,1}(\vec{\mathbf{r}})) + \alpha_{2\to 1}(\vec{\mathbf{r}}) (\phi_2(\vec{\mathbf{r}},t) - \phi_{eq,2}(\vec{\mathbf{r}})) \\ \frac{1}{v_2} \frac{\partial}{\partial t} \phi_2(\vec{\mathbf{r}},t) &= \Sigma_r(\vec{\mathbf{r}},t) \phi_1(\vec{\mathbf{r}},t) + \left[\vec{\nabla} \cdot D_2(\vec{\mathbf{r}},t) \vec{\nabla} - \Sigma_{a,2,wox}(\vec{\mathbf{r}},t) \right] \phi_2(\vec{\mathbf{r}},t) \\ &+ \alpha_{1\to 2}(\vec{\mathbf{r}}) (\phi_1(\vec{\mathbf{r}},t) - \phi_{eq,1}(\vec{\mathbf{r}})) + \alpha_{2\to 2}(\vec{\mathbf{r}}) (\phi_2(\vec{\mathbf{r}},t) - \phi_{eq,2}(\vec{\mathbf{r}})) \\ &- \sigma_X X(\vec{\mathbf{r}},t) \phi_2(\vec{\mathbf{r}},t) \\ &\frac{\partial}{\partial t} I(\vec{\mathbf{r}},t) &= \gamma_I \Sigma'_{f,1}(\vec{\mathbf{r}},t) \phi_1(\vec{\mathbf{r}},t) + \gamma_I \Sigma'_{f,2}(\vec{\mathbf{r}},t) \phi_2(\vec{\mathbf{r}},t) - \lambda_I I(\vec{\mathbf{r}},t) \\ &\frac{\partial}{\partial t} X(\vec{\mathbf{r}},t) &= \gamma_X \Sigma'_{f,1}(\vec{\mathbf{r}},t) \phi_1(\vec{\mathbf{r}},t) + \gamma_X \Sigma'_{f,2}(\vec{\mathbf{r}},t) \phi_2(\vec{\mathbf{r}},t) + \lambda_I I(\vec{\mathbf{r}},t) - \lambda_X X(\vec{\mathbf{r}},t) \\ &- \sigma_X X(\vec{\mathbf{r}},t) \phi_2(\vec{\mathbf{r}},t). \end{split}$$

$$\begin{split} \mathbf{XS INPUT DATA} \\ D_1(\vec{\mathbf{r}}) \quad D_2(\vec{\mathbf{r}}) \\ &\Sigma_{f,1}(\vec{\mathbf{r}}) \quad \nabla \Sigma_{f,2}(\vec{\mathbf{r}}) \\ &\Sigma_{r}(\vec{\mathbf{r}}) \end{split}$$

$$\begin{split} \mathbf{Xer}(\vec{\mathbf{r},t) = \sum_{r,r} (\vec{\mathbf{r},r)} \nabla \Sigma_{r,2}(\vec{\mathbf{r},r)} \\ &\Sigma_r(\vec{\mathbf{r},r) \end{matrix}$$

Problem definition



My workflow





Simulating a reactor





Xenon poisoning

Evolution chain of Xenon-135



Xenon poisoning





Xenon poisoning $\bullet \phi_1(\vec{r},t)$ $\phi_2(\vec{r},t)$ U-235 $\implies X(t) = \frac{\lambda_I}{\lambda_I - \lambda_X} \left(e^{-\lambda_X t} - e^{-\lambda_I t} \right) I_0 + e^{-\lambda_X t} X_0$ I-135 9000 8000 6.7 h 9.2 h Xe-135 7000 6000 5000 4000 3000 **Evolution chain of Xenon-135** 2000 fission 1000 0 20 100 120 160 40 60 80 140 180 ββ time [h] 135₁ ¹³⁵Cs 6.7 h 9.2 h (n, y) ¹³⁶Xe

Xenon poisoning



Fig. 4.10 Evolution of the poisoning due to ${}^{135}Xe$ after the start of the reactor (t=0), after a reactor scram (t=100 h), and after a reactor restart (t=130 h) (the horizontal dashed lines represent the equilibrium poisonings).

Xenon oscillations







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Highlight from the development process

Simulation to induce Xenon oscillations: Core-Averaged Quantities (dt = 900[s])



- Time-evolution is done with the Crank-Nicolson method,
- Asymptotically stable (A-stable)
- This means that the method is numerically stable for arbitrarily large time-steps...

From a certain perspective, this is not an error/mistake, but is in fact the correct solution according to Crank-Nicolson...

- When I handed in my thesis for grading and I had officially finished my work on the project, I still wasn't done with the problem.
- 1. Numerical oscillations fascinated me, wanted to find general solution.
- 2. Arbitrary XS-perturbation
- 3. Adaptive time-stepping
- So after I finished my thesis, I completely rewrote my entire code from scratch, and fixed/implemented points 1-3.
- It turned out that this required roughly as much time and effort as the entire original master's thesis project.
- Lines of code: 4485
- I would happily tell you everything about this!